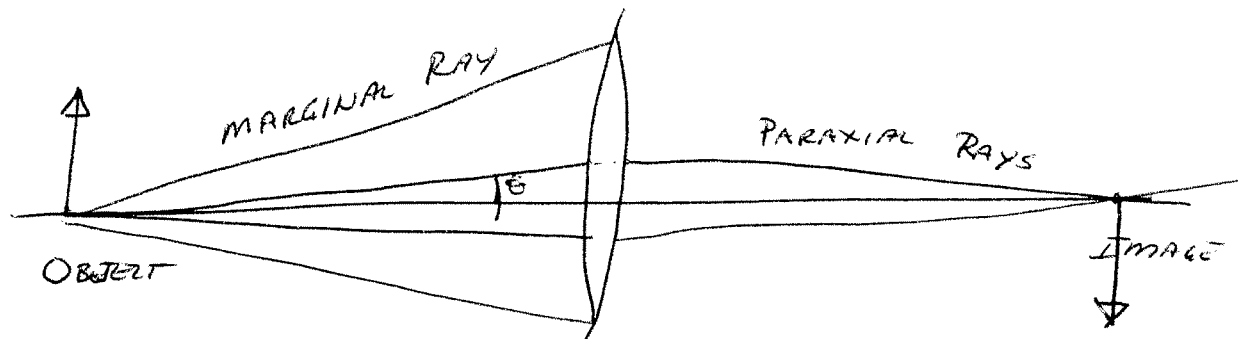


10 FEBRUARY 2010

①

RAY OPTICS MODEL OF IMAGING

FIND (LOCATE) IMAGES, PARAXIAL APPROXIMATION
MAGNIFICATIONS \rightarrow QUALITY (ABERRATIONS)



LOGARITHMS

1970s \rightarrow COMPUTERS, OSLO, CODE V

HERO OF ALEXANDRIA _N LIGHT RAY TRAVELS SHORTEST PATH

FERMAT - LIGHT RAY TRAVELS PATH ~~TO~~ THAT TAKES SHORTEST

OPTICAL PATH LENGTH $\phi = \frac{2\pi}{\lambda'} z = \frac{2\pi}{\lambda/n} z = \cancel{2\pi} z$

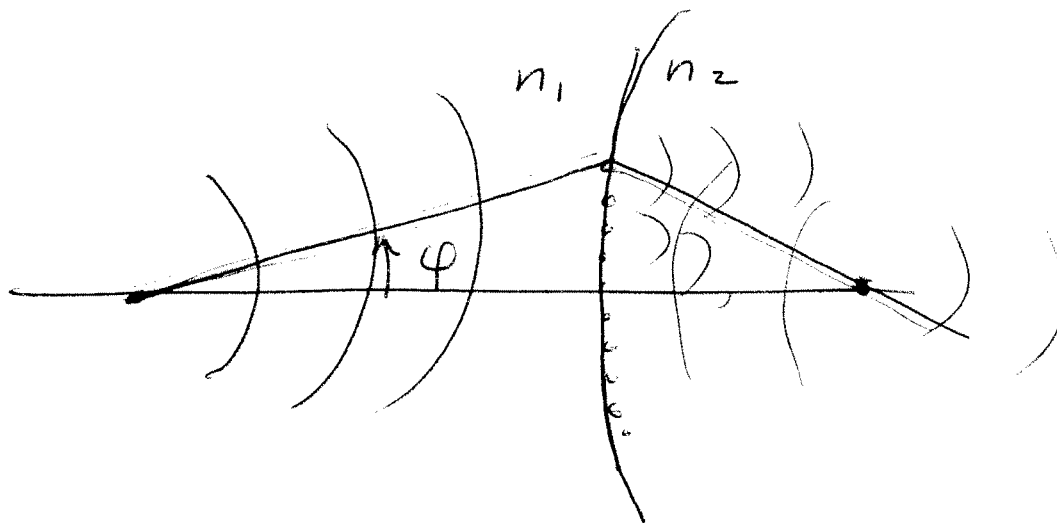
$$\phi = \frac{2\pi (nz)}{\lambda_0}$$

OPTICAL PATH LENGTH = nz

OPL = DISTANCE LIGHT TRAVELS IN VACUUM IN SAME TIME
AS WOULD TRAVEL z IN INDEX n

$$OPL > z$$

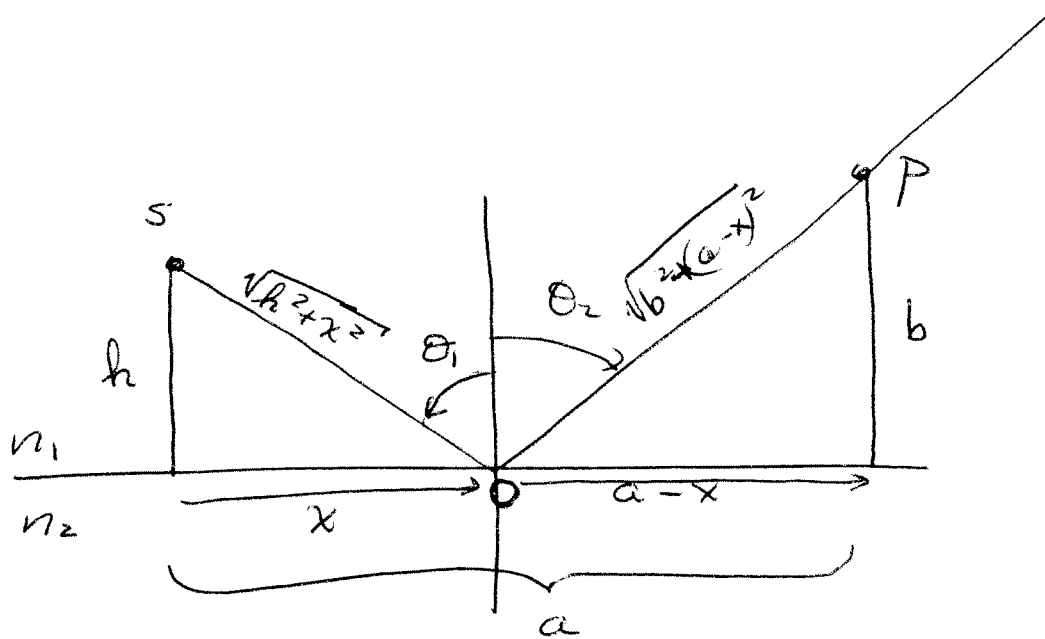
$$\frac{dOPL}{d\phi} = 0$$



FERMAT'S PRINCIPLE AND REFLECTION

(SAME INDEX)

2/10-③



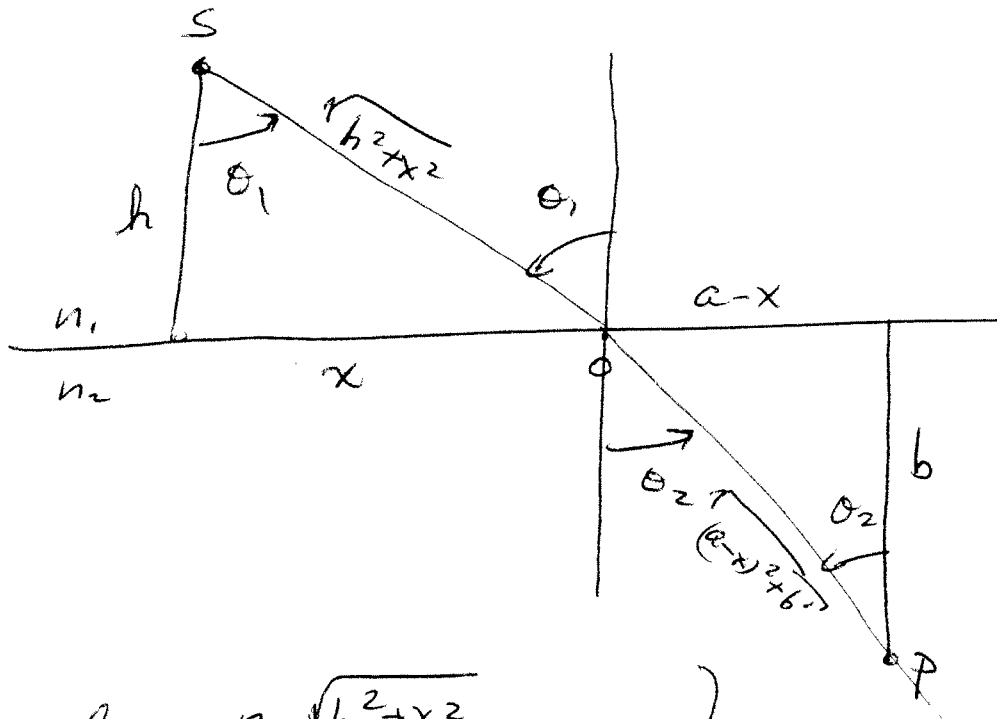
$\theta_1 > 0$
 $\theta_2 < 0$

} AS DRAWN

$$\left. \begin{aligned}
 l_1 &= n_1 \sqrt{h^2 + x^2} \\
 l_2 &= n_1 \sqrt{b^2 + (a-x)^2}
 \end{aligned} \right\} \begin{aligned}
 OPL &= l_1 + l_2 \\
 \frac{dOPL}{dx} &= 0 = \frac{dOPL}{dx} \cdot \frac{dx}{d\theta}
 \end{aligned}$$

$$\Rightarrow \sin \theta_1 = \sin(-\theta_2) \Rightarrow \theta_2 = -\theta_1$$

2/10 - ④



$$l_1 = n_1 \sqrt{h^2+x^2}$$

$$l_2 = n_2 \sqrt{b^2+(a-x)^2}$$

}

$$OPL = l_1 + l_2$$

$$= n_1 \sqrt{h^2+x^2} + n_2 \sqrt{b^2+(a-x)^2}$$

$$\frac{d}{dx} OPL = n_1 \frac{1}{2\sqrt{h^2+x^2}} \cdot 2x + n_2 \frac{1-2(a-x) \cdot (-1)}{2\sqrt{b^2+(a-x)^2}} \text{ (1)}$$

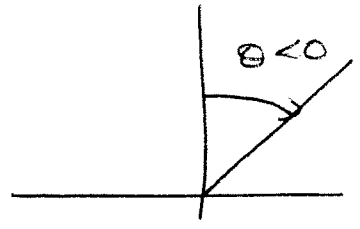
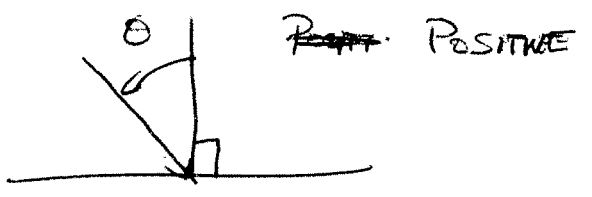
$$= n_1 \frac{x}{\sqrt{h^2+x^2}} + n_2 \frac{a-x}{\sqrt{b^2+(a-x)^2}}$$

$$= n_1 \sin \theta_1 - n_2 \sin \theta_2 = 0$$

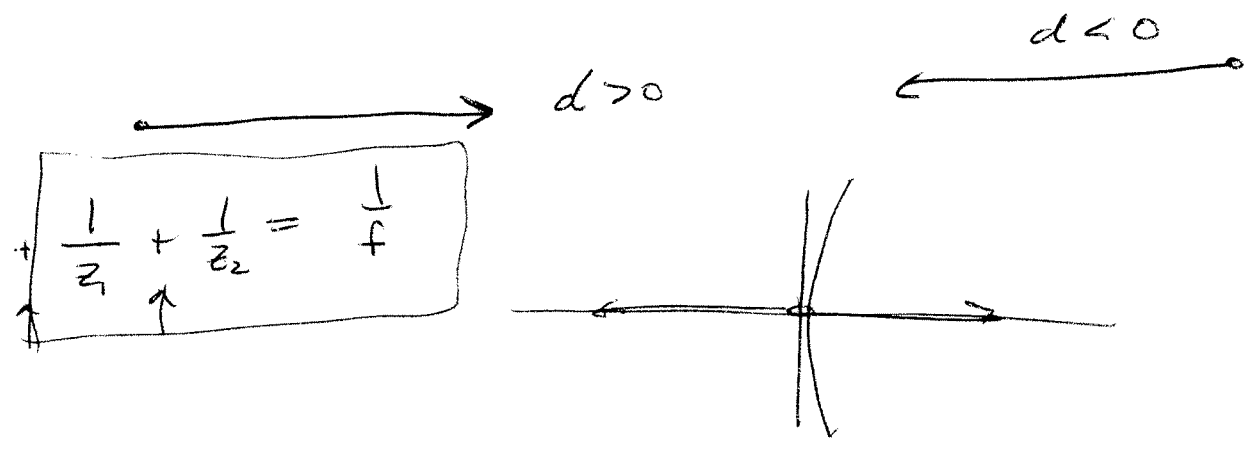
$$\frac{d}{dx} (OPL) = 0 \Rightarrow n_1 \sin \theta_1 = n_2 \sin \theta_2$$

SNELL'S LAW FOR REFRACTION

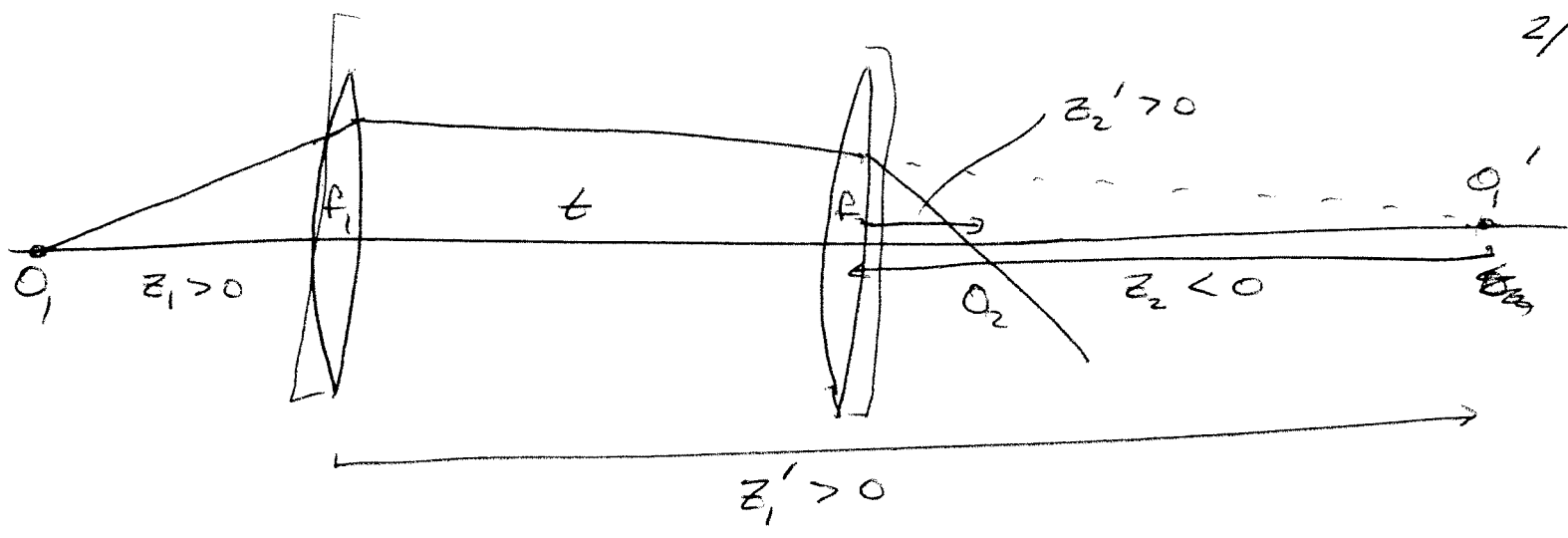
SIGN CONVENTIONS



DISTANCE
(DIRECTED DISTANCE)



2/10 - (6)



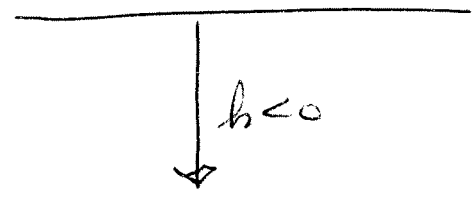
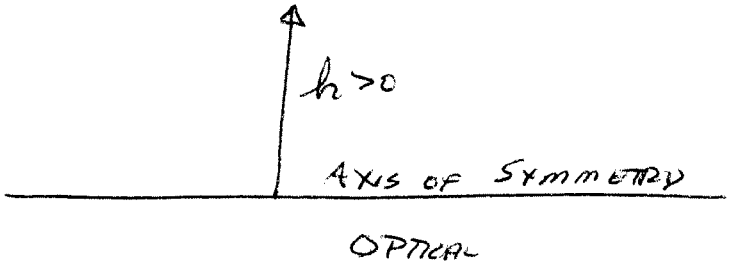
$$\frac{1}{s_1} + \frac{1}{s_2} = \frac{1}{f_{\text{eff}}}$$

effective OBJECT DISTANCE
 FROM OBJECT TO OBJECT-SPACE PRINCIPAL POINT

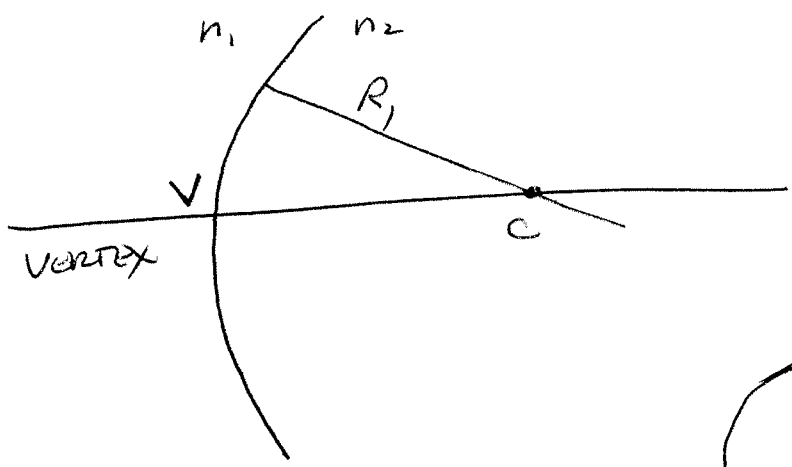
eff IMAGE DISTANCE
 FROM H_2 TO O_2

2/10 - (7)

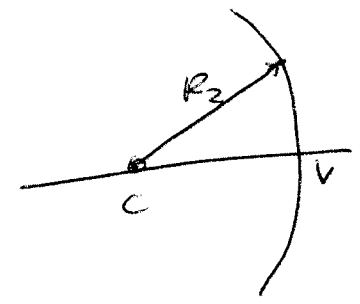
HEIGHT



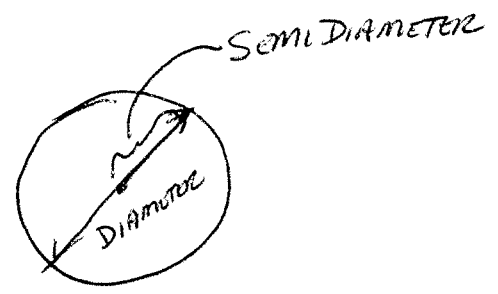
RADIi OF CURVATURE



$$\overline{VC} = R_1 > 0$$



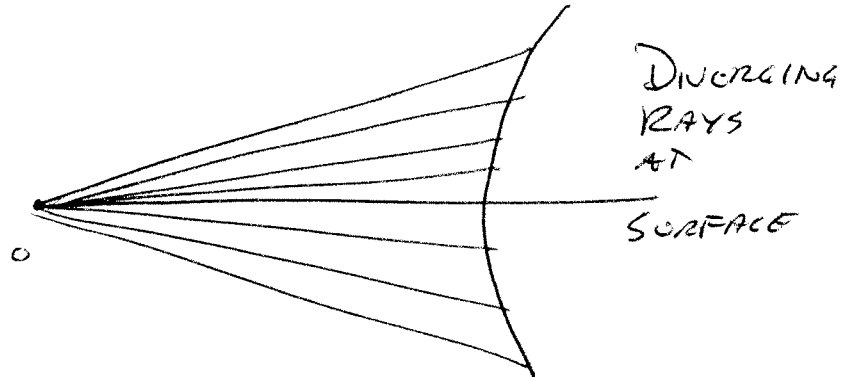
$$R_2 < 0$$



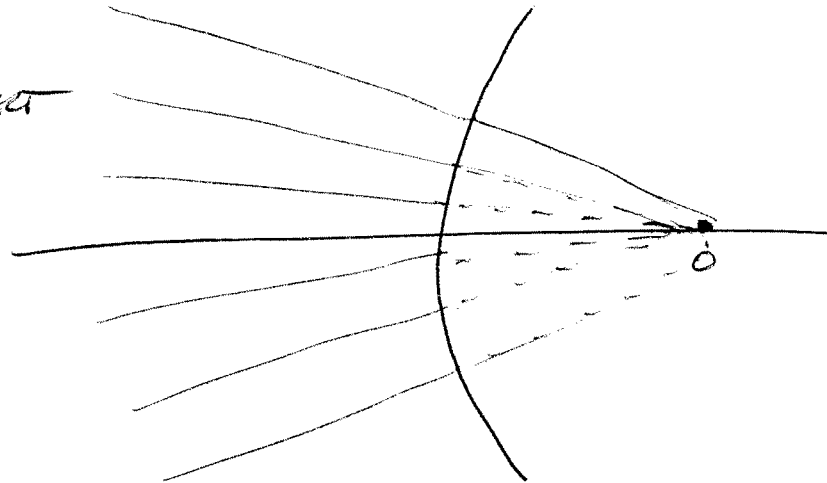
"QUALITY" OF OBJECT & IMAGE
REAL, & VIRTUAL

2/10 - (8)

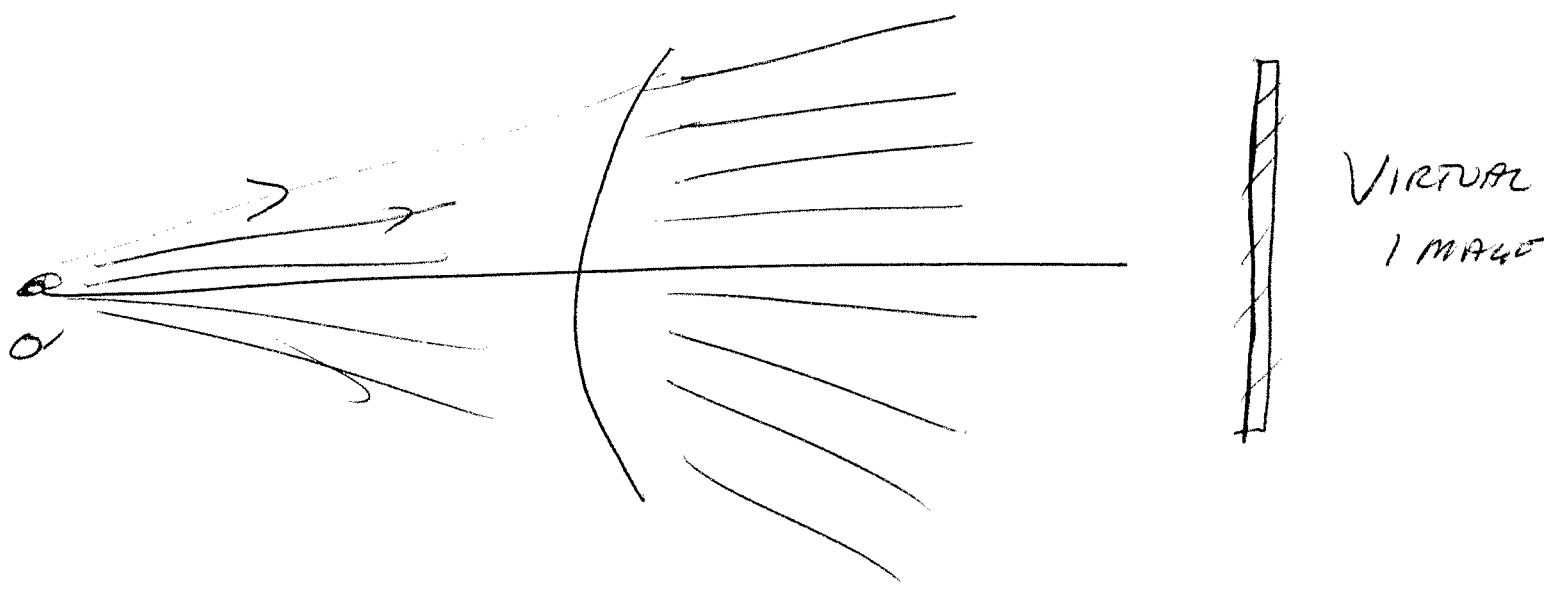
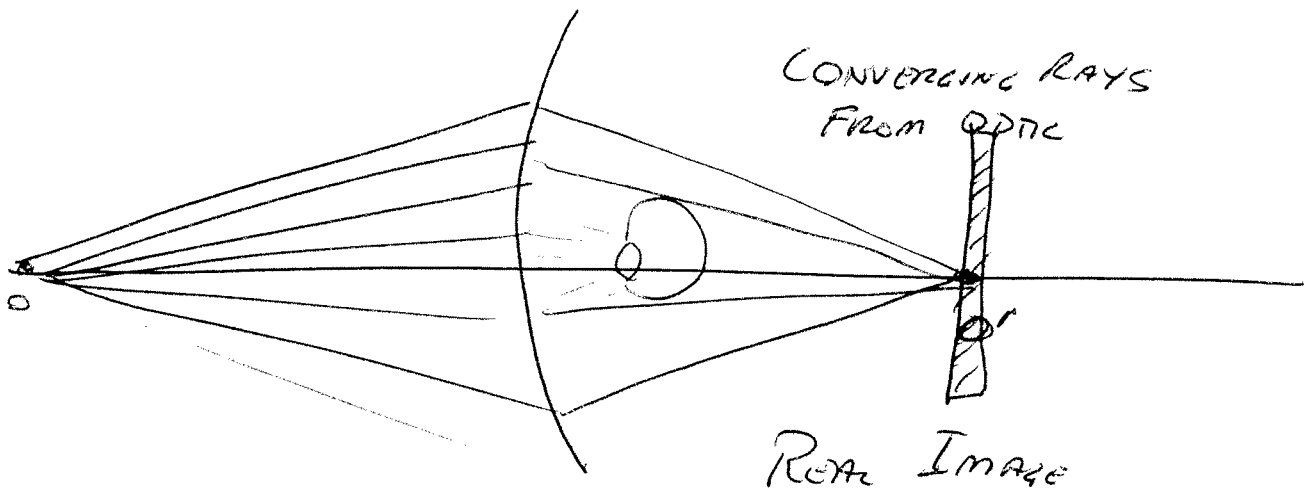
REAL OBJECT



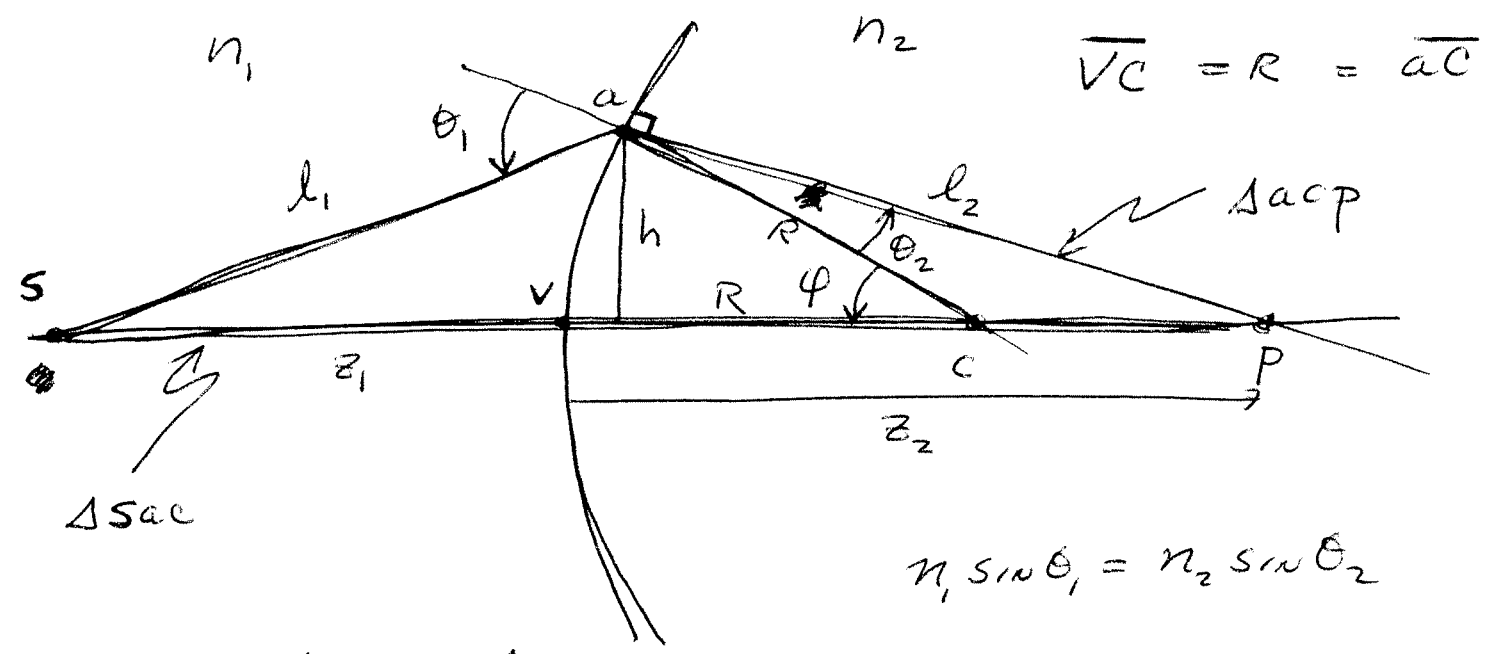
VIRTUAL OBJECT



2/10 - (9)



REFRACTION FROM SINGLE SURFACE



$$n_1 \sin \theta_1 = n_2 \sin \theta_2$$

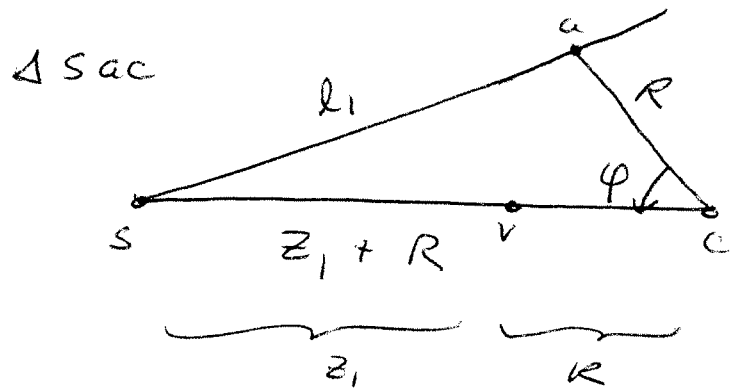
$$OPL = n_1 l_1 + n_2 l_2$$

$$\frac{d}{d\varphi} (OPL) \Rightarrow (1) f[z_1, l_1, n_1, z_2, l_2, n_2]$$

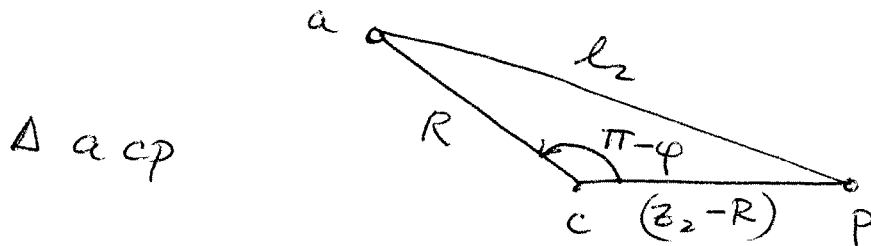
(2) IF $\varphi \approx 0$, $z_1 \approx l_1$, $z_2 \approx l_2 \Rightarrow$ PARAXIAL

- Δsac

$\sin \varphi \approx \tan \varphi \approx \varphi \Rightarrow$ LINEAR EXPRESSION



$$l_1^2 = R^2 + (z_1 + R)^2 - 2R(z_1 + R)\cos\varphi$$



$$l_2^2 = R^2 + (z_2 - R)^2 - 2R(z_2 - R)\cos(\pi - \varphi)$$

$$\cos(\pi - \varphi) = \cos\pi\cos\varphi + \sin\pi\sin\varphi = -\cos\varphi$$

$$l_2^2 = R^2 + (z_2 - R)^2 + 2R(z_2 - R)\cos\varphi \Rightarrow l_2 = \sqrt{R^2 + (z_2 - R)^2 + 2R(z_2 - R)\cos\varphi}$$

$$l_1^2 = R^2 + (z_1 + R)^2 - 2R(z_1 + R)\cos\varphi \quad l_1 = \sqrt{\quad}$$

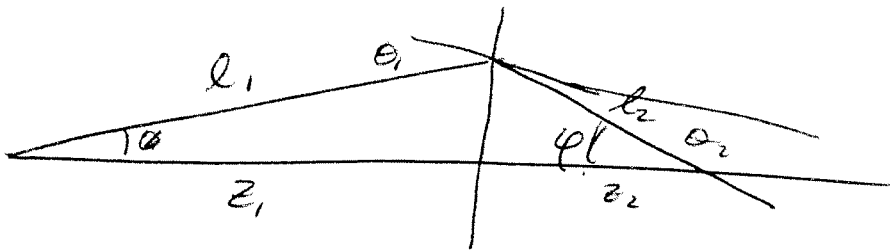
$$OPL = n_1 l_1 + n_2 l_2$$

$$\frac{dOPL}{d\varphi} = n_1 \frac{1}{2\sqrt{\quad}} + 2R(z_1 + R)\sin\varphi + n_2 \frac{1}{\sqrt{\quad}} - 2R(z_2 - R)\sin\varphi$$

2/10 - (12)

$$\frac{n_1}{l_1} + \frac{n_2(R-z_2)}{l_2} = 0$$

$$\frac{n_1}{l_1} + \frac{n_2}{l_2} = \frac{1}{R} \left(\frac{n_2 z_2}{l_2} - \frac{n_1 z_1}{l_1} \right)$$



$$\frac{l_2}{z_2} = \frac{1}{\cos \phi}$$

IF $\phi \approx 0$, $\cos \phi \approx 1 - \frac{\phi^2}{2} + \dots$

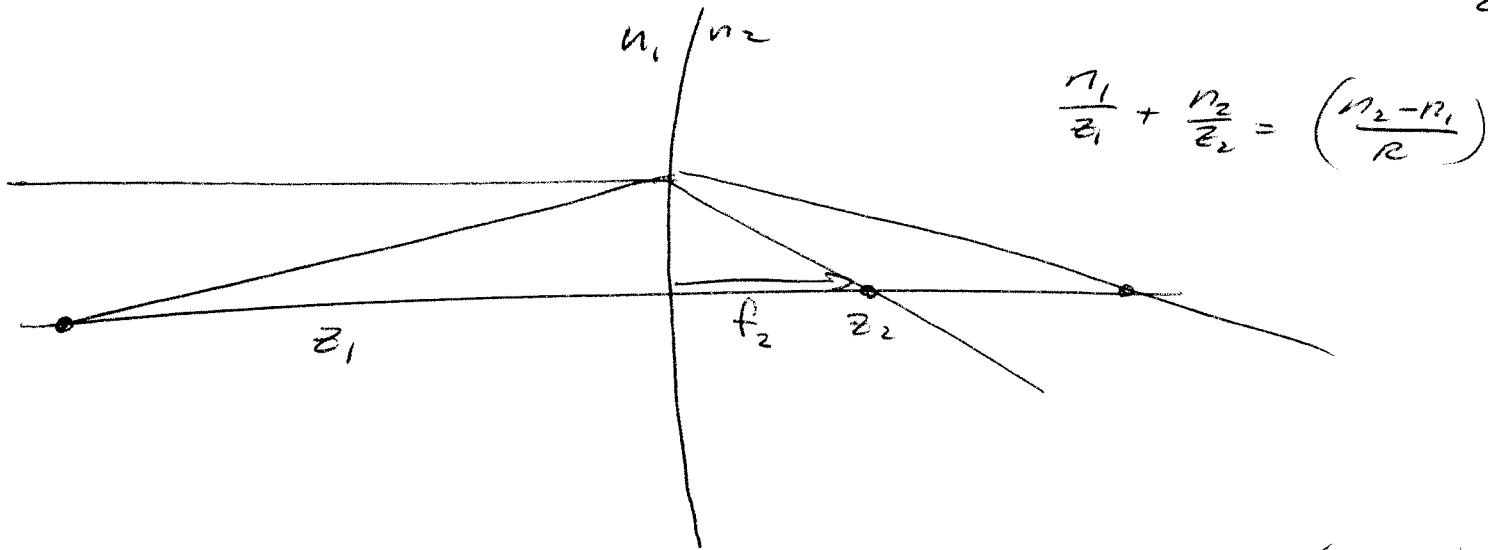
$$\left. \begin{array}{l} l_2 \sim z_2 \\ l_1 \sim z_1 \end{array} \right\} \Rightarrow$$

$$\frac{n_1}{z_1} + \frac{n_2}{z_2} = \frac{1}{R} (n_2 - n_1)$$

$$\sin \phi \sim \phi$$

PARAXIAL APPROX FOR REFRACTION FROM SINGLE SURF

2/10 - (13)



$$\frac{n_1}{z_1} + \frac{n_2}{z_2} = \left(\frac{n_2 - R_1}{R} \right)$$

$$(1) \quad z_1 = \infty \quad \frac{n_1}{\infty} + \frac{n_2}{z_2} = \frac{n_2 - R_1}{R_1} \Rightarrow z_2 = R_1 \cdot \left(\frac{n_2}{n_2 - R_1} \right)$$

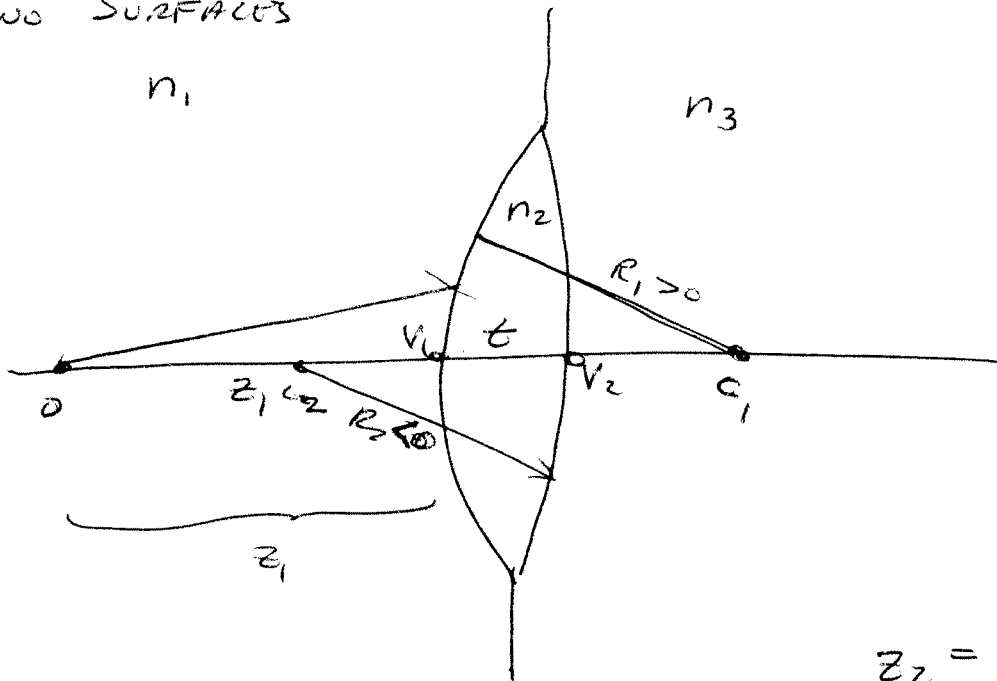
$$f_2 = \left(\frac{n_2}{n_2 - R_1} \right) R$$

$$(2) \quad z_2 = \infty \quad \frac{n_1}{z_1} + 0 = \frac{n_2 - R_1}{R_1} \Rightarrow z_1 = f_1 = R_1 \cdot \left(\frac{n_1}{n_2 - R_1} \right)$$

$$\boxed{\frac{f_1}{f_2} = \frac{n_1}{n_2}}$$

TWO SURFACES

2/10 (14)



$$(1) \quad \frac{n_1}{z_1} + \frac{n_2}{z_1'} = \frac{n_2 - n_1}{R_1}$$

$$(2) \quad \frac{n_2}{z_2} + \frac{n_3}{z_2'} = \frac{n_3 - n_2}{R_2}$$

$$t = 0 \Rightarrow z_1' = -z_2$$

$$z_2 = t - z_1'$$

$$z_2 = -z_1' \text{ IF } t = 0 \text{ (THIN LENS)}$$

$$z_1' = t - z_2$$

THIN LENS

$$\frac{n_1}{z_1} + \left(\frac{n_2}{-z_2} \right) = \frac{n_2 - n_1}{R_1}$$

$$\left(\frac{n_2}{z_2} \right) + \frac{n_3}{z_2'} = \frac{n_3 - n_2}{R_2}$$

$$\frac{n_1}{z_1} + \frac{n_3}{z_2'} = \frac{n_2 - n_1}{R_1} + \frac{n_3 - n_2}{R_2} = -\frac{n_1}{R_1} + \frac{n_3}{R_2} + n_2 \left(\frac{1}{R_1} - \frac{1}{R_2} \right)$$

\uparrow \uparrow
 OBJECT IMAGE

$$\frac{n_1}{z_1} + \frac{n_3}{z_2'} = -\frac{n_1}{R_1} + \frac{n_3}{R_2} + n_2 \left(\frac{1}{R_1} - \frac{1}{R_2} \right)$$

IN AIR $n_1 = n_3 = 1$

$$\begin{aligned} \frac{1}{z_1} + \frac{1}{z_2'} &= -\frac{1}{R_1} + \frac{1}{R_2} + n_2 \left(\frac{1}{R_1} - \frac{1}{R_2} \right) \\ &= -\left(\frac{1}{R_1} - \frac{1}{R_2} \right) + n_2 \left(\frac{1}{R_1} - \frac{1}{R_2} \right) \end{aligned}$$

2/10 - (16)

THIN LENS, 3 MEDIA

$$\frac{n_1}{z_1} + \frac{n_3}{z_2'} = -\frac{n_1}{R_1} + \frac{n_3}{R_2} + n_2 \left(\frac{1}{R_2} - \frac{1}{R_1} \right)$$

IN AIR

$$\frac{1}{z_1} + \frac{1}{z_2'} = (n_2 - 1) \left(\frac{1}{R_1} - \frac{1}{R_2} \right)$$

LENSMAKER'S EQUATION
(FOR THIN LENS)

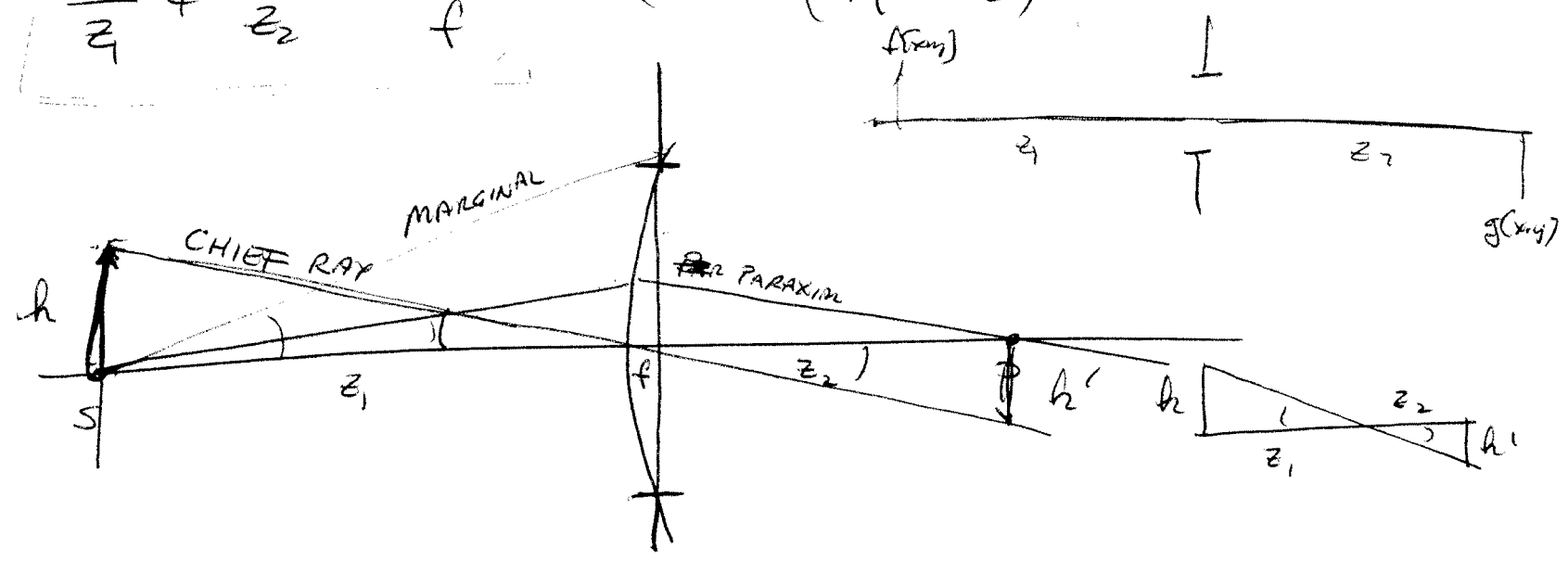
$z_2' \equiv z_2$

$$\frac{1}{z_1} + \frac{1}{z_2} \equiv \frac{1}{f}$$

FROM DIFFRACTION

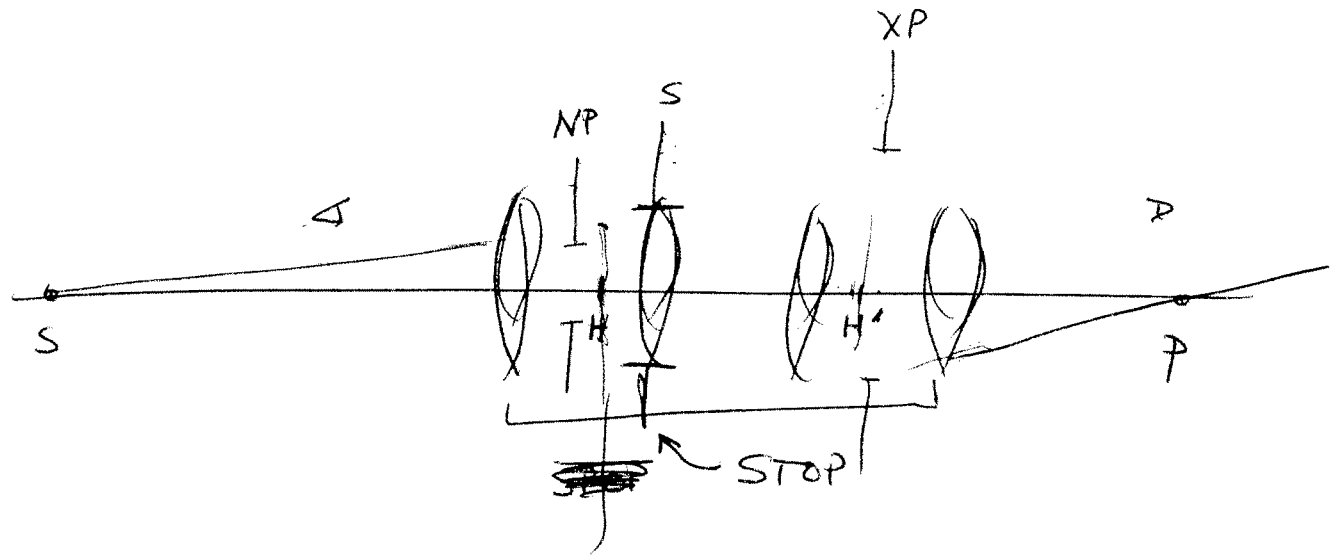
$$\frac{1}{f} = (n_2 - 1) \left(\frac{1}{R_1} - \frac{1}{R_2} \right)$$

$$\frac{1}{z_1} + \frac{1}{z_2} = \frac{1}{f} = (n_2 - 1) \left(\frac{1}{R_1} - \frac{1}{R_2} \right)$$



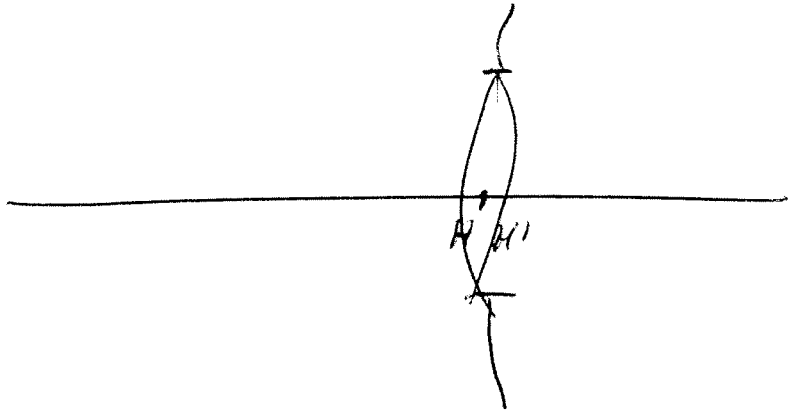
- CHIEF RAY - EDGE OF OBJECT \rightarrow CENTER OF LENS \rightarrow EDGE OF IMAGE (PUPIL)
- PARAXIAL RAY - CENTER OF OBJECT \rightarrow INTERSECT LENS \rightarrow CENTER OF IMAGE
- MARGINAL RAY - SCALED REPLICIA OF PARAXIAL
- EDGE OF APERTURE STOP \Leftrightarrow ENTRANCE PUPIL \Leftrightarrow EXIT PUPIL

$$\boxed{\frac{h'}{h} = -\frac{z_2}{z_1}} = M_T \quad M_\theta$$

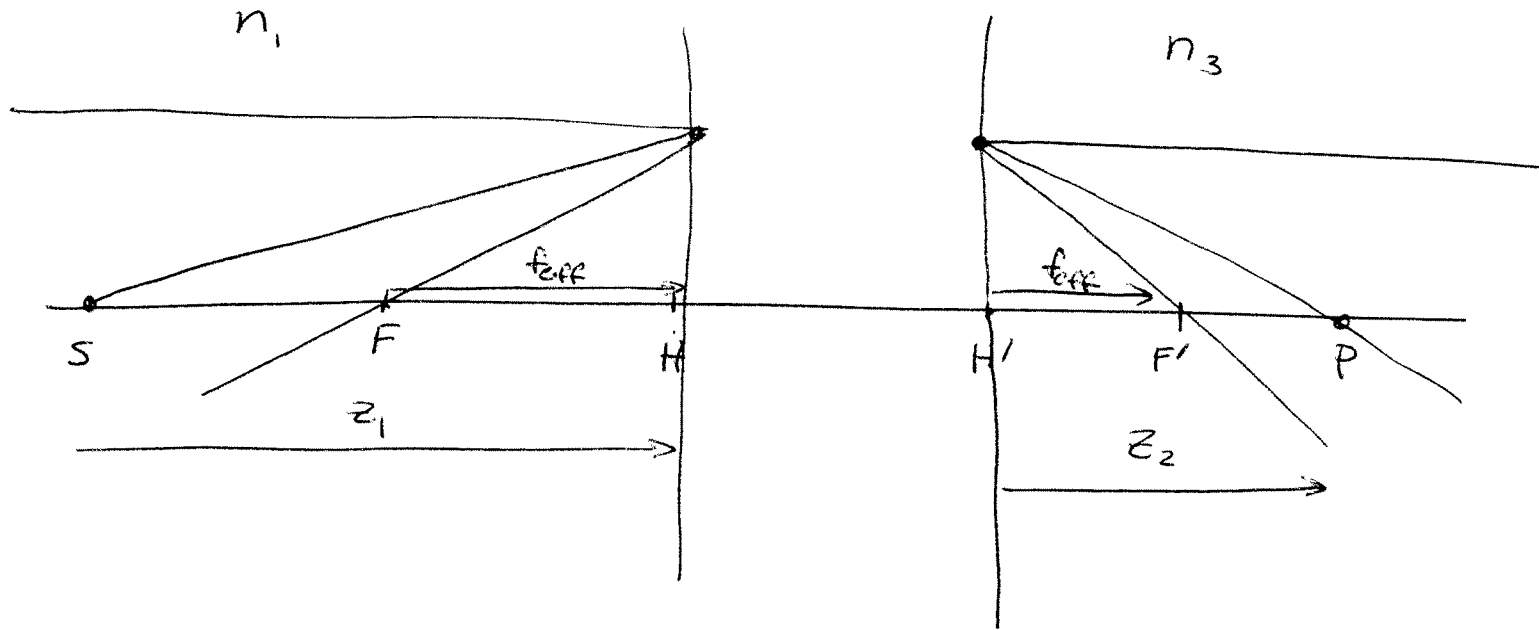


OBJECT SPACE
PRINCIPAL PLANE

H' IS IMAGE OF A
WITH $M_T = +1$
↑



2/10 - (A)



$$\frac{1}{z_1} + \frac{1}{z_2} = \frac{1}{\underline{\underline{f_{eff}}}}$$

